

Predictive Thermodynamic Model for Intrusion of Electrolyte Aqueous Solutions in Nanoporous Materials

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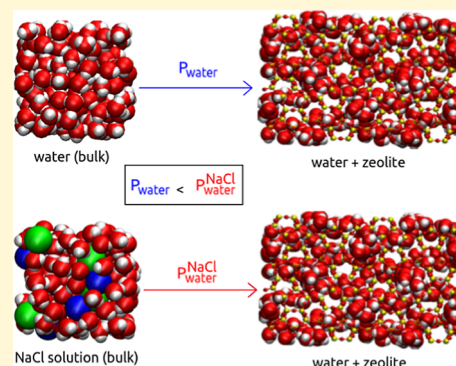


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ABSTRACT: We performed Monte Carlo simulations in the osmotic ensemble in three representative hypothetical pure-silica zeolites that are silicalite-1, chabazite, and faujasite for which the adsorption isotherm of water has been calculated from grand canonical Monte Carlo simulations. Monte Carlo moves in the osmotic ensemble to insert electrolyte reveal that the ions do not penetrate the zeolites at water intrusion pressure because they are better solvated in bulk for low-diameter pore zeolites, due to lower ion solvation in the nanopores. Then, the chemical potential of water in electrolyte solutions has been calculated and it highlights the same dependency in pressure as the chemical potential of pure water. From these conclusions, we propose a thermodynamic model that revisits the law of osmotic pressure in order to predict the intrusion pressure in zeolites taking into account the nature of electrolytes in solution.



INTRODUCTION

One of the most important challenges of material science consists in the elaboration of devices that can efficiently generate, store, and transfer energy. In particular, intrusion and extrusion of a nonwetting liquid in porous lyophobic systems is a promising technology investigated first by Eroshenko and coworkers,^{1–8} where the nonwetting liquid penetrates the pores under high pressure, resulting in conversion of mechanical energy into fluid–solid interface energy. When the pressure is released, the mechanical energy can be restored upon the release of the fluid. Historically, intrusion of water in pure-silica zeolites (also called “zeosils”) has been first reported in 2001⁹ and represents the starting point of subsequent intrusion and extrusion experiments performed on various zeolites.^{10–19} Later, Tzani and coworkers²⁰ discovered that replacing water by electrolyte solutions was an effective way to increase mechanical energy stored in zeolites, because of the shift of intrusion pressure toward higher values. For instance, it was shown that intrusion of highly concentrated LiCl solution (~20 M) in silicalite-1 increases intrusion pressure from 96 to 280 MPa, resulting in an increase of stored energy from 10 to 31 J/g. Since this pioneering work, the nature and concentration of electrolyte on the intrusion and extrusion pressure and energetic properties of zeolites has been widely investigated.^{21–37} In addition to zeolites, that are the scope of this work, we note that intrusion and extrusion of pure water and electrolyte solutions have also been investigated in other microporous materials, such as metal–organic frameworks ZIF-8,^{38–41} ZIF-71,⁴² and other ZIF materials,^{43–47} as well as MAF-6.⁴⁸

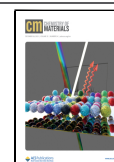
Although the mechanism of water intrusion in hydrophobic microporous materials has been highlighted by grand canonical Monte Carlo (GCMC) simulations,^{12,49,50} the mechanism of electrolyte intrusion is still under debate; it is characterized by an increase of intrusion pressure that depends both on electrolyte nature and concentration. Several hypotheses have been proposed such as ion desolvation,²⁰ osmotic effect,⁴¹ confinement effect^{51,52} or increase of solid–liquid interfacial tension.^{53,54} Recently, it has been shown that intrusion of NaCl electrolyte solution in chabazite and LTA-type zeolites occurs in two steps.^{21,30} First, only water molecules penetrate into the nanocages at 44 and 36 MPa in chabazite and LTA-type zeolites, respectively. Then, the ions penetrate at a much higher pressure of 260 and 140–240 MPa, respectively. This is supported by previous Monte Carlo (MC) simulations performed by Zamfir and coworkers,⁵⁴ where NaCl electrolyte penetrates a two-dimensional planar hydrophobic nanopores once the water has been intruded inside it. The initial step consisting of the intrusion of only water molecules is crucial for energy storage applications. Thus, the dependence of the intrusion pressure with the nature and concentration of electrolyte requires further investigation, which is the object of this work by relying on our recent implementation of molecular simulations with an osmostat for electrolyte aqueous

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solutions.⁵⁵ Briefly, the osmostat is based on a hybrid MC move using nonequilibrium molecular dynamics, named nonequilibrium candidate Monte Carlo (NCCM), proposed by Nilmeier⁵⁶ and later applied by Ross and coworkers⁵⁷ to sample the distribution of NaCl electrolyte around biomolecules. We previously calculated the chemical potential of ion exchange $\Delta\mu_{C_nA_m}(P)$ in the semigrand canonical ensemble for “alchemically” transforming $(n + m)$ water molecules chosen randomly into an electrolyte unit C_nA_m (where C^{m+} and A^{n-} denote respectively the cation and the anion electrolyte) in bulk electrolyte solution at fixed concentration. We used a modified version of the Widom insertion method except that the work performed during the alchemical transformation $W_{(n+m)H_2O \rightarrow C_nA_m}$ (referred to as the “alchemical work” to be noted $W_{C_nA_m}$) is taken into account, instead of the difference of energy between the initial and the final steps of the alchemical transformation. This chemical potential used in combination with NCCM moves to insert or delete ions at a constant number of particles in the system defines the osmotic ensemble, where the fictitious reservoir is an electrolyte solution at a concentration imposed by the chemical potential.

In this work, we investigated the intrusion of electrolyte solutions in three representative hypothetical zeolites (silicalite-1, chabazite, and faujasite) chosen for their increasing channel/cage diameter and the availability of experimental data. First, we calculated the isotherm of pure water intrusion by GCMC simulations in each of these three zeolites. Then, using the configurations of water-loaded zeolites at equilibrium at different pressures, we apply our osmostat⁵⁵ and found that the alchemical work associated with ion insertion in the zeolites is much lower than in the bulk, leading to very low probabilities of intrusion. Assuming that water penetrates first the porous materials as observed experimentally for chabazite and LTA-type zeolites,^{21,30} we then revisited the law of osmotic pressure and derived an analytical model to predict intrusion pressure of electrolyte solutions in zeolites for various electrolytes and concentrations.

MODEL AND METHODS

Systems and Force Field. The systems we studied are three representative pure silica zeolites: silicalite-1 (MFI topology), chabazite (CHA topology), and faujasite (FAU topology). For channel-type zeolite such as silicalite-1, the intrusion pressure of water depends on the channel diameter d_{ch} while for cage-like zeolites (chabazite and faujasite), it correlates with the cage diameter d_{ca} .⁵⁶ We have chosen these zeolites because of the increasing “characteristic diameter”: in increasing order, silicalite-1 ($d_{ch} = 5.40$ Å), chabazite ($d_{ca} = 7.37$ Å) and faujasite ($d_{ca} = 11.24$ Å).⁵⁸ The zeolites are generally considered rigid, and it is assumed that no structural or chemical changes occur upon electrolyte intrusion or extrusion. We used the crystal structure determined by Olson⁵⁹ for silicalite-1, the chabazite structure is that reported by Calligaris⁶⁰ while faujasite structure is that published by Hriljac.⁶¹

We note here that pure-silica faujasite has not been synthesized so far, and even experimental faujasites with high Si/Al ratios exhibit a significant number of aluminum atoms. The pure-silica faujasite used in this work is thus a speculative model based on the atomic coordinates that correspond to crystallographic data for a faujasite with a Si/Al ratio of 2.61. These unit cell parameters of the structures are given in Table 1, and their structures are represented in Figure 1. In this study, we simulated respectively a box of four, 12, and one unit cells for silicalite-1, chabazite, and faujasite in order to have large enough systems to avoid side effects due to applications of periodic boundary conditions.

Table 1. Cell Parameters of Zeolites Used in this Work

	<i>a</i> (Å)	<i>b</i> (Å)	<i>c</i> (Å)	α (deg)	β (deg)	γ (deg)
silicalite-1 ⁵⁹	20.070	19.920	13.420	90	90	90
chabazite ⁶⁰	9.459	9.459	9.459	94.07	94.07	94.07
faujasite ⁶¹	24.258	24.258	24.258	90	90	90

We chose the force field developed for silicalite-1 by Desbiers and coworkers⁴⁹ to model interactions for zeolites in this study. This force field is tailored to reproduce intrusion pressure of TIP4P water around ~ 100 MPa, as observed in experiments.⁶² Water molecules are modeled with the rigid TIP4P model⁶³ and the electrolytes are represented as charged beads that differ by their Lennard–Jones parameters and charges. We considered the following monovalent electrolytes which are LiCl, NaCl, KCl, RbCl, CsCl, KF, KBr, and KI. We also explored the following divalent electrolytes to probe the influence of charge ion: MgCl₂, CaCl₂, SrCl₂, and BaCl₂. The details of the force field are given in Tables S1–S4.^{64,65}

We used Lorentz–Berthelot mixing rules for cross-terms in Lennard–Jones potential and Ewald summation to account efficiently for electrostatic interactions. We used a cutoff of 8.0 Å for both the Lennard–Jones potential and the separation between the real space and reciprocal space in the Ewald summation.

MC Simulations. Adsorption isotherms of pure water in zeolites were computed with GCMC simulations using the RASPA simulation package.⁶⁶ We screened several values of the chemical potential of the fictitious water reservoir⁴⁹ to compute the number of adsorbed water molecules by using the relationship between chemical potential of water and hydrostatic pressure $\mu_{water}(P)$.⁴⁹ In order to explore phase space, translation, rotation, and swap moves were applied to water molecules, in a ratio of 1:1:2, respectively. Each simulation consists of 2×10^5 equilibration cycles followed by 10^5 production cycles, during which average quantities were calculated.

In order to probe electrolyte insertion in zeolites in the osmotic ensemble, we used our recently released implementation version of the NCCM move⁵⁵ with a relative probability set to 10^{-3} . The NCCM move consists of $\mathcal{T}=200$ steps, each one involving a perturbation of the system through interpolation of nonbonded parameters of the chosen molecules to be transformed, followed by 200 MD relaxation steps with a time step of 1 fs in the NVE ensemble. All simulations used a Nosé–Hoover thermostat, setting the temperature at 300 K. In addition, translations were performed both on ions and water while rotations were applied only to water molecules, in a ratio of 1:1:1 respectively. Each simulation was performed until 1000 values of the alchemical work had been gathered.

Then, we calculated the chemical potential $\Delta\mu_{C_nA_m}(P)$ in bulk electrolyte solutions containing 150 particles (composition given in Table S5), as in our previous study⁵⁵ but for pressure ranging from 0.006 to 1000 MPa. Because concentration depends explicitly on the volume of the solution, it is more convenient to use molality as the relevant metric.⁵⁴ This quantity will be required as input to set up the osmostat in zeolites filled with water molecules at different pressure. At each value of pressure, the simulation was performed until 400 values of the alchemical work had been gathered to construct the $\Delta\mu_{C_nA_m}(P)$ relationship.

Finally, we also used the adapted NCCM moves to calculate the chemical potential of water, as detailed in ref 55, and applied it to compute the chemical potential of water in electrolyte solutions $\mu_{water}^{C_nA_m}(P)$ of various molalities (Table S5) for pressure ranging from 0.006 to 1000 MPa. At each value of pressure, the simulation was performed until 400 values of the work associated with a single water insertion had been gathered to construct the $\mu_{water}^{C_nA_m}(P)$ relationship.

Molecular Dynamics Simulations. Because of the sequential nature of the RASPA software, we used GROMACS⁶⁷ to perform MD simulations in the (N, P, T) ensemble to determine the density of systems with the same composition but four times bigger (600

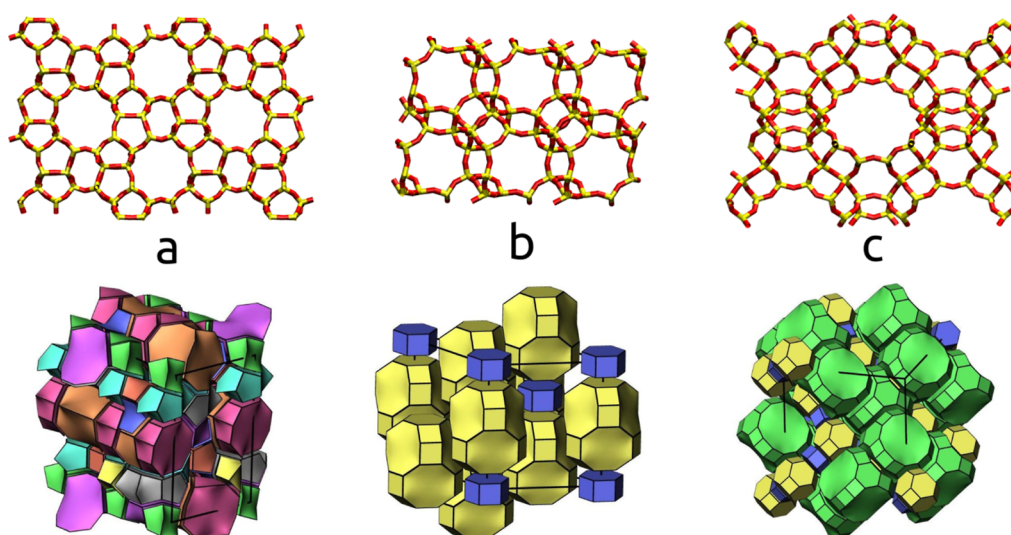


Figure 1. (a) View of four unit cells of silicalite-1 along the crystallographic *b* axis. (b) View of 12-unit cells of chabazite along the crystallographic *b* axis. (c) View of one-unit cell of faujasite along the crystallographic (1 1 0) direction. Bottom: three corresponding tilings of the zeolite nets.

particles) than those presented in Table S5. From these simulations, we extracted the average density and deduced the volume of the fixed cubic box to perform MC simulations in RASPA and calculate $\Delta\mu_{C_rA_m}(P)$ and $\mu_{\text{water}}^{C_rA_m}(P)$ as explained above. The raw data presenting the relationship between applied pressure and density in electrolyte solution are given in the Supporting Information.

RESULTS AND DISCUSSION

Monte Carlo Simulations of Water Intrusion/Extrusion in Zeolites. Figure 2 reports the adsorption and

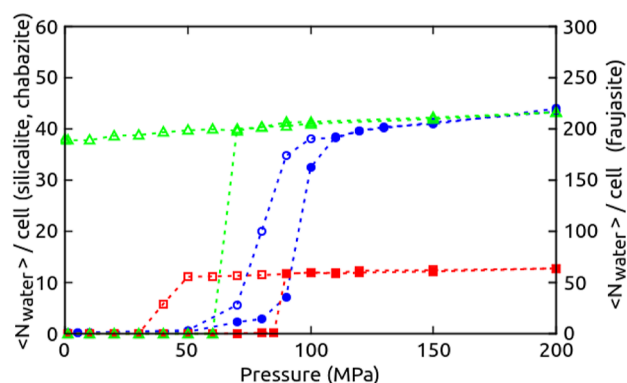


Figure 2. Water intrusion and extrusion isotherms computed through GCMC simulations at 300 K. Filled symbols refer to intrusion, while open symbols refer to extrusion. Blue circles: silicalite-1; red squares: chabazite; green triangles: faujasite.

desorption isotherms of TIP4P water in silicalite-1, chabazite, and faujasite zeolites. Given that the force field used for zeolites has been specifically designed to reproduce TIP4P water adsorption isotherm in silicalite-1 zeolite, we confirm that the adsorption isotherm calculated in this work for silicalite-1 is consistent with both previous GCMC simulations^{49,62,68} and experiments,⁹ as shown in Figure S1. Also, the intrusion pressures are similar for silicalite-1 and chabazite with values of respectively 95 and 90 MPa while for the faujasite, it drops to 65 MPa. We do not expect a perfect agreement between the simulated and experimental intrusion isotherms of water in chabazite and faujasite, given that intrusion pressure is very

sensitive to the choice of force field and other structural features such as silanol defects. For instance, the experimental intrusion pressure of water in pure silica chabazite is about 32 MPa, lower than in our work.¹³

Our results are in qualitative agreement with the Washburn equation,⁶⁹ as higher intrusion pressure is correlated with the smaller cage or channel diameter along our series of zeolites. Also, we analyzed the thermodynamics of water intrusion by calculating the adsorption heat q through the relationship⁷⁰

$$q = RT + \frac{\langle U^{\text{tot}}N \rangle - \langle U^{\text{tot}} \rangle \langle N \rangle}{\langle N^2 \rangle - \langle N \rangle^2} \quad (1)$$

where U^{tot} is the sum of host–guest and guest–guest interactions. In Figures S2 and S4, we report the evolution of the heat of intrusion and extrusion in each zeolite. The hydrophobic nature of the zeolites is clearly visible from the heat of adsorption at very low loading, which is dominated by interaction of water with the zeolite structure. In each case, the heat of adsorption is comprised between 20 and 30 kJ/mol, which is much lower than the bulk vaporization enthalpy of water (44 kJ/mol for TIP4P water at 300 K). After water intrusion, the heat of adsorption becomes higher than the bulk vaporization enthalpy of water, due to the formation of a dense liquid-like water phase in the pores of the zeolites. In this case, the heat of adsorption is dominated by interaction between water molecules.

Electrolyte Intrusion in Zeolites at Different Water Loading.

The process of water intrusion in zeolites is the initial step for further probing the electrolyte intrusion in these materials. We use the final configuration of the zeolite–water system at 200 MPa for chabazite and faujasite where 13.25 and 211 water molecules are adsorbed per cell, respectively, while for silicalite-1, the final system containing 53 water molecules per cell at 400 MPa is considered. We also investigated electrolyte intrusion at other water loadings. For proof-of-concept, we do not perform GCMC simulations for these cases but relax systems of zeolite–water at chosen loading by MC simulation in the *NVT* ensemble for probing the influence of water loading on the electrolyte intrusion. Consequently, we investigate loadings of 5, 10, 15, 20, 30, and 58.5 water

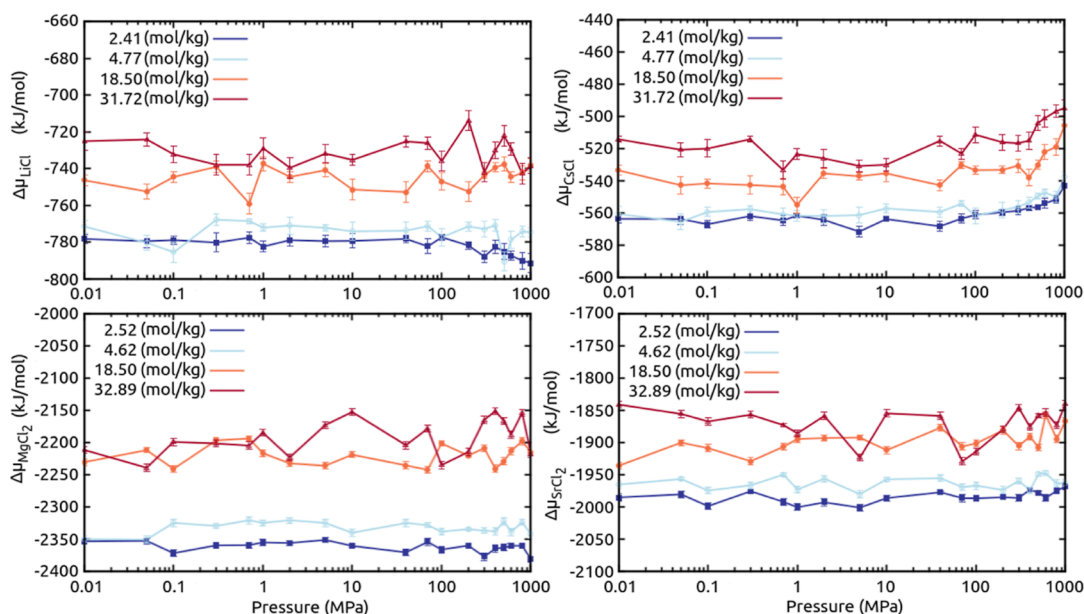


Figure 3. Chemical potential of ion exchange $\Delta\mu_{C_rA_m}(P)$ as a function of pressure. Top-left: evolution of $\Delta\mu_{LiCl}(P)$. Top-right: evolution of $\Delta\mu_{CsCl}(P)$. Bottom-left: evolution of $\Delta\mu_{MgCl_2}(P)$. Bottom-right: evolution of $\Delta\mu_{SrCl_2}(P)$.

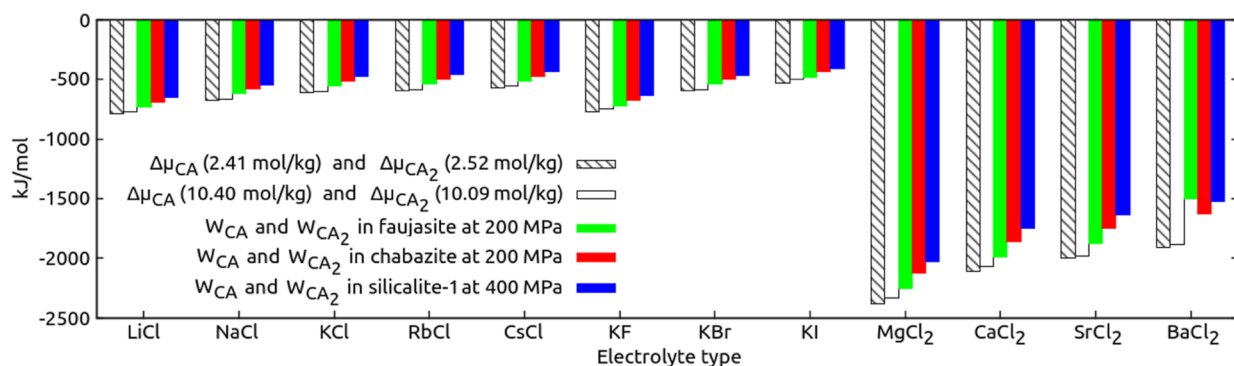


Figure 4. Histograms of the alchemical work W_{CA} for monovalent and W_{CA_2} for divalent-cation electrolytes associated with the intrusion of a single electrolyte unit in faujasite (green), chabazite (red), and silicalite-1 (blue). The chemical potential of ion exchange $\Delta\mu_{CA}$ for monovalent and $\Delta\mu_{CA_2}$ for divalent-cation electrolytes in the bulk for molalities of respectively 2.41, 10.40, and 2.52, 10.09 mol/kg are represented as dashed and white histograms.

molecules per cell in silicalite-1; for chabazite, systems characterized by 1.33, 2.66, 4, 5.33, 6.66, 8.33, 15, and 16.66 water molecules per unit cell are investigated. Finally, faujasite contains 20, 40, 80, 120, 215, 260, and 275 water molecules per unit cell.

It is required to calibrate the chemical potential $\Delta\mu_{C_rA_m}(P)$ as performed in our former work⁵⁵ for a wide range of pressure to assess electrolyte intrusion at 200 MPa in chabazite and faujasite and at 400 MPa in silicalite-1. These calculations are computationally expensive so that we investigated only two representative monovalent electrolytes, which are LiCl and CsCl since Li^+ is the smallest cation ($\sigma_{Li^+} = 1.505 \text{ \AA}$) while Cs^+ is the largest one ($\sigma_{Cs^+} = 3.883 \text{ \AA}$) among the alkali-chloride electrolytes. For similar reasons, we chose two divalent electrolytes, which are $MgCl_2$ and $SrCl_2$. The evolution of $\Delta\mu_{C_rA_m}(P)$ is reported in Figure 3. For all cases, the chemical potential of ion exchange fluctuates around a mean value over the pressure investigated. It is understandable because no new particles are inserted in the system; only water molecules are

replaced by ions. However, for CsCl, the chemical potential becomes more positive for pressures higher than 200 MPa. Consequently, we assume that chemical potential of ion exchange does not depend on the pressure up to 200 MPa, allowing us to use the chemical potential calculated in our former study⁵⁵ in this work.

The evolution of the alchemical work associated with the intrusion of an electrolyte unit in zeolites filled with water at 200 MPa (chabazite and faujasite) and 400 MPa (silicalite-1) is presented in Figure 4 while row values and error estimation can be found in Tables S6 and S7.

The alchemical work is the lowest in the silicalite-1, and increases for chabazite and faujasite, which is consistent with silicalite-1 channel diameter and chabazite and faujasite cage diameter. We deduce that a lower pore size is associated with a mediocre solvation of the ions, because the lack of available space does not allow water molecules to properly form solvation shells around the ions. The alchemical work is lower for every electrolyte investigated compared to $\Delta\mu_{C_rA_m}(P)$ calculated for electrolyte bulk solution at different molalities,

but it is necessary to be more quantitative by calculating the associated probability for insertion of an electrolyte unit in the zeosils. We recall from our previous work⁵⁵ that the probability for accepting an electrolyte unit is written as follows

$$P_{\text{acc}} = \min \left(1, \frac{\prod_{i=0}^{m+n-1} (N_{\text{H}_2\text{O}} - i)}{\prod_{j=1}^n (N_{\text{C}_r^{\text{A}_m}} + j) \prod_{k=1}^m (N_{\text{A}^{\text{r}}} + k)} e^{-\beta(W_{\text{C}_r^{\text{A}_m}} - \Delta\mu_{\text{C}_r^{\text{A}_m}})} \right) \\ = \min(1, N_{\text{H}_2\text{O}}(N_{\text{H}_2\text{O}} - 1) e^{-\beta(W_{\text{C}_r^{\text{A}_m}} - \Delta\mu_{\text{C}_r^{\text{A}_m}})}) \quad (2)$$

We estimate the probability of ion intrusion by using the raw values of the alchemical work and the chemical potential reported in Tables S6 and S7. At bulk molality of 2.41 mol/kg for monovalent electrolytes CA, the probability of ion intrusion is about $\sim 10^{-6}$, $\sim 10^{-13}$ and $\sim 10^{-18}$ – 10^{-20} for faujasite, chabazite, and silicalite-1, respectively. The probability of ion intrusion for divalent-cation electrolytes CA_2 at bulk molality of 2.52 mol/kg is lower than for monovalent electrolytes with probabilities of $\sim 10^{-18}$, $\sim 10^{-40}$ and $\sim 10^{-60}$ respectively, because it is less favorable to solvate simultaneously three ions in the zeosils than an ion pair in case of monovalent electrolytes. For bulk electrolyte at high molalities (i.e., at 10.40 mol/kg for monovalent electrolytes), the probability of electrolyte intrusion increases for all zeosils but remains insignificant for silicalite-1 ($\sim 10^{-16}$ – 10^{-17}) and chabazite ($\sim 10^{-10}$ – 10^{-12}). On the contrary, the probability of electrolyte intrusion in faujasite becomes significant ($\sim 10^{-4}$ – 10^{-1}), indicating that electrolyte may penetrate the zeosil at such concentration. Finally, in the presence of divalent electrolytes, the insertion probability in the three zeosils also increases but remains low so that no electrolyte may be intruded as well. In Figure S8, we present the distribution of the alchemical work for inserting a first NaCl unit in silicalite-1, chabazite, and faujasite. The histogram queue for silicalite-1 and chabazite reveals that several intrusions of NaCl electrolyte are associated with insertion probabilities P_{acc} of $\sim 10^{-1}$ for bulk molality of 10.09 mol/kg. However, after eventual intrusion of a NaCl pair, it is unlikely that the pair remains in the framework because alchemical work associated with the reverse move for transforming the NaCl into water molecules (denoted as $W_{-\text{NaCl}}$ in our former work⁵⁵) is the opposite of W_{NaCl} resulting in a very high probability ($P_{\text{del}} \propto \exp[-\beta(\Delta\mu_{\text{C}_r^{\text{A}_m}} - W_{\text{C}_r^{\text{A}_m}})]$) to remove the ion pair.

In experiments, NaCl electrolyte at concentration of 2 M penetrates chabazite when only 7 water molecules per cell are adsorbed, which is lower than loading of 14 water molecules obtained by GCMC simulations (Figure 2). Therein, we calculated the alchemical work required to solvate a single NaCl pair in zeosils at different water loadings. The results are reported in Figure S9 and reveal a lower alchemical work, associated with a worst solvation of the ions due to the low amount of water present in the zeosils. On the contrary, at very high amount of water molecules, the alchemical work also diminishes for faujasite and chabazite because the dense fluid in cages cannot accommodate easily the intruded ions. Our simulations does not catch electrolyte intrusion in chabazite as shown in experiments²¹ which may be attributed to the absence of defects in our models of zeosil or even other phenomenon that are not taken into account using classical

force field such as reactivity of water with zeolites. Nonetheless, it was shown by in situ X-ray diffraction experiments on NaCl aqueous solutions intrusion in pure silica chabazite²¹ and LTA-type zeosil³⁰ that only the water molecules penetrate first (or at low pressure) into the pores, and we will work henceforth within this hypothesis.

Chemical Potential of Water in Electrolyte Solutions.

Assuming that only water molecules but no electrolytes penetrate the zeosils, it is required to probe the evolution of water chemical potential in electrolyte solutions $\mu_{\text{water}}^{\text{C}_r^{\text{A}_m}}(P)$. In the case of pure water, there are three ways to derive the $\mu_{\text{water}}(P)$ relationship. From mercury porosimetry experiments, Porcheron and Monson⁷¹ integrated the Gibbs–Duhem equation while Chempath and coworkers⁷² computed the chemical potential of the vapor with equilibrium to the liquid phase at a given temperature by using the Peng–Robinson equation of state. The third approach consists in using molecular simulation to calculate water chemical potential as performed by Desbiens et al.⁴⁹ for the rigid TIP4P water model. A set of (N, P, T) simulations were performed in order to obtain the relationship between pressure and density. The chemical potential as a function of the density is subsequently calculated by using $[\mu_{\text{water}}(P), V, T]$ simulations so that the density is used as an intermediate quantity easy to compute in order to obtain the $\mu_{\text{water}}(P)$ relationship. In our work, another approach is proposed: we performed (N, P, T) MD simulations to retrieve the density that is used to fix the simulation box in RASPA to run subsequent (N, V, T) simulations where the NCMC move is used to compute $\mu_{\text{water}}(P)$ with our adapted version of the Widom insertion technique. The comparison between different methods to calculate $\mu_{\text{water}}(P)$ is reported in Figure 5.

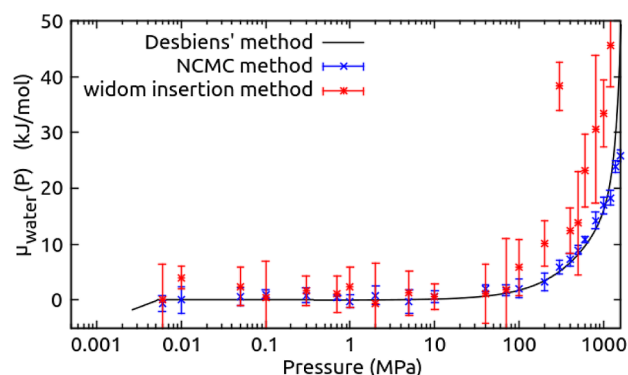


Figure 5. Chemical potential of TIP4P water was estimated by three methods. Black curve: Desbiens' method. Blue points: Widom insertion method combined with NCMC move. Red points: standard Widom insertion method.

For the sake of comparison, we run the same (N, V, T) simulation but instead use Widom insertion moves to estimate the $\mu_{\text{water}}(P)$ relationship. It is clear that this last approach is not suited for the computation of the chemical potential in such dense fluid because the probability of intrusion is very low due to an overestimation of the chemical potential at high pressure induced by interpenetration of sample molecule with other water molecules.⁷³ On the contrary, by using the NCMC move, the system is relaxed during insertion of the sample molecule and the chemical potential calculated with the modified Widom technique⁵⁵ is in agreement with those

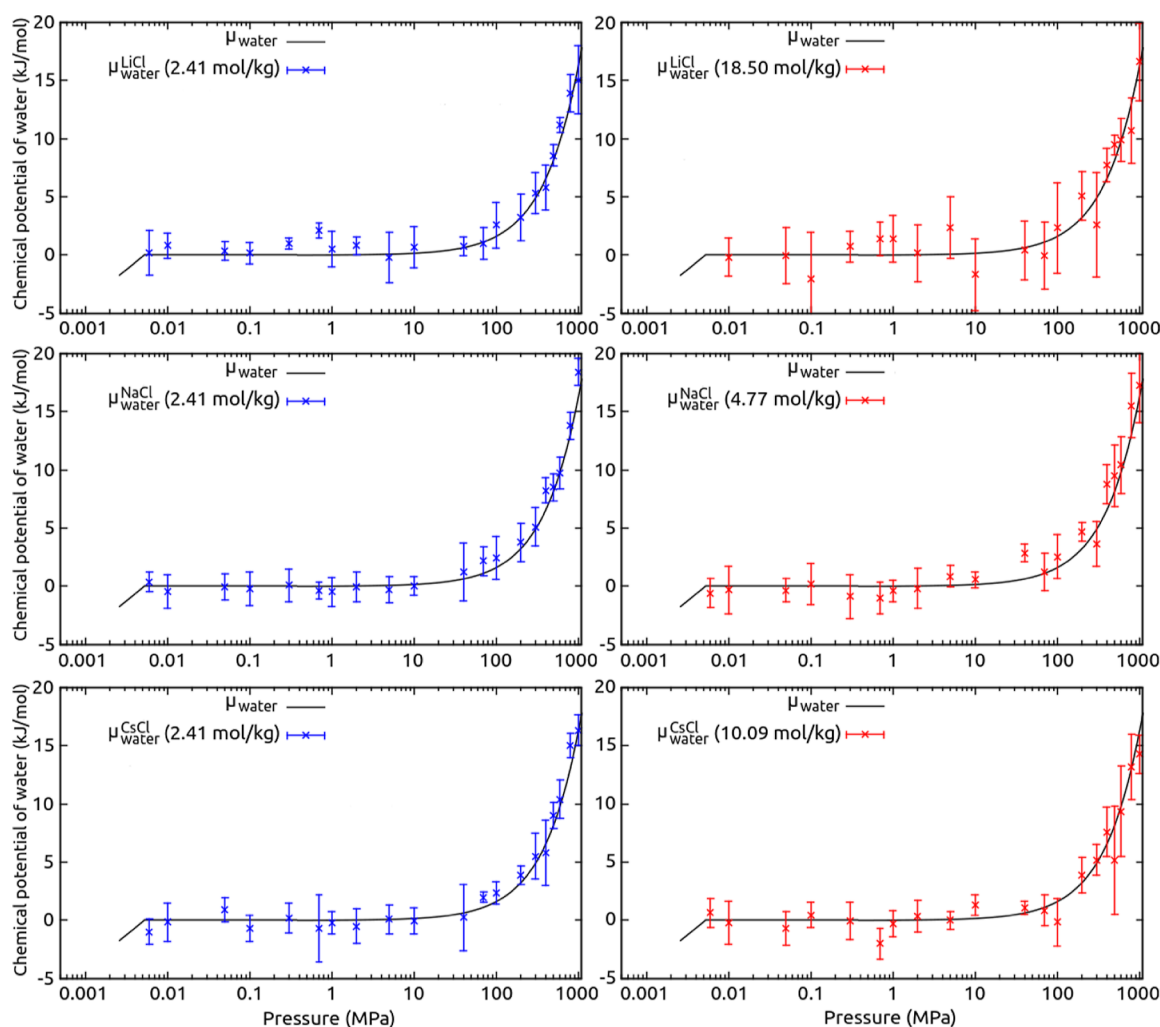


Figure 6. Chemical potential of TIP4P water in electrolyte solutions. Top: $\mu_{\text{water}}^{\text{LiCl}}(P)$; middle: $\mu_{\text{water}}^{\text{NaCl}}(P)$; bottom: $\mu_{\text{water}}^{\text{CsCl}}(P)$ at different molalities. The chemical potential of pure water is shown as black line in each plot for comparison.⁴⁹

calculated by Desbiens and co-workers. In addition, we verify that both methods yield the same slope of chemical potential of pure water as a function of pressure [e.g., same molar volume $v_{\text{water}}(P)$], as shown in Figure S5.

Although the method proposed by Desbiens and coworkers is suitable for pure water, we did not apply it to determine the $\mu_{\text{water}}^{\text{C}_{n\text{A}_m}}(P)$ relationship for electrolyte solutions. Although there is no trouble in performing (N, P, T) simulation of electrolyte solutions to obtain the density as a function of pressure, the drawback comes from the $(\mu_{\text{water}}^{\text{C}_{n\text{A}_m}}(P), V, T)$ simulations where $\mu_{\text{water}}^{\text{C}_{n\text{A}_m}}(P)$ needs to be determined as a function of density. The chemical potential $\mu_{\text{water}}^{\text{C}_{n\text{A}_m}}(P)$ as input parameter dictates the evolution of the number of water molecules in the system except that the number of electrolyte units must also vary accordingly to keep a constant electrolyte concentration. In order to address such issue, we used the NCMC move to compute $\mu_{\text{water}}^{\text{C}_{n\text{A}_m}}(P)$ as this method has been successfully applied to calculate $\mu_{\text{water}}(P)$ for pure TIP4P water. The results for LiCl, NaCl, and CsCl electrolyte units at two different molalities are presented in Figure 6.

Here, the chemical potential of water in electrolyte solutions $\mu_{\text{water}}^{\text{C}_{n\text{A}_m}}(P)$ has been computed starting from 0.006 MPa, which

is slightly higher than the vapor pressure of pure TIP4P water (0.0053 MPa) and vapor pressure of any electrolyte solution in this work. We do not focus on pressure below this value because the evolution of the vapor pressure of electrolyte solution in this range of pressure will be discussed later in the paper. The common trend is that the chemical potential of water in electrolyte solutions shows the same dependency in pressure as the chemical potential in pure water and this observation holds also for divalent-cation electrolytes ($\mu_{\text{water}}^{\text{MgCl}_2}(P)$ and $\mu_{\text{water}}^{\text{BaCl}_2}(P)$) as shown in Figure S10).

In order to further support our results, we calculate⁷⁴ the molar volume of water $v_{\text{water}}^{\text{C}_{n\text{A}_m}}(P)$ in electrolyte solutions up to ~ 40 MPa from experimental electrolyte densities $\rho_{\text{sol}}(P)$ and partial molar volume of electrolytes $v_{\text{C}_{n\text{A}_m}}(P)$ using the following relationship

$$v_{\text{water}}^{\text{C}_{n\text{A}_m}}(P) = \frac{M_{\text{water}} - \rho_{\text{sol}}(P)x_{\text{C}_{n\text{A}_m}}\left(\frac{M_{\text{water}}}{M_{\text{C}_{n\text{A}_m}}}\right)v_{\text{C}_{n\text{A}_m}}(P)}{\rho_{\text{sol}}(P)x_{\text{water}}} \quad (3)$$

where M_{water} and $M_{\text{C}_{n\text{A}_m}}$ are respectively the molar mass of water and electrolyte and x_{water} and $x_{\text{C}_{n\text{A}_m}}$ are the mass fraction of water and electrolyte in solution. In Figures S6 and S7, we plot $v_{\text{water}}^{\text{C}_{n\text{A}_m}}(P)$ for monovalent (LiCl, NaCl, KCl) and divalent

(MgCl₂, CaCl₂) electrolytes up to molalities of 5 mol/kg as well as molar volume of pure water extracted from NIST data. It is clear from experiments that the partial molar volume of water in electrolyte solutions is the same as the molar volume of pure water, irrespective of the concentration and valency of the electrolyte, which is in agreement with Figure 6.

In the following section, we will assume that the chemical potential of water in the presence of electrolyte will have the same dependency on pressure as that for pure water.

Law of Osmotic Pressure Revisited. The main result obtained from the simulations in the osmotic ensemble is that no ions penetrate the zeolites, only water molecules. The nonpenetration of ions is therefore used as the main hypothesis for the revision of the law of osmotic pressure presented in this section, by taking account explicitly the nature and concentration of the electrolyte solution. We previously demonstrated that the chemical potential of water in electrolyte solutions displays the same dependency in pressure as for pure water but differ in their vapor pressure—that depends on the nature and concentration of the electrolyte.

Foremost, let us recall the link between chemical potential $\mu_{\text{water}}(P)$, fugacity f and fugacity coefficient ϕ for TIP4P water. In Figure S11, we present the chemical potential of pure TIP4P water $\mu_{\text{water}}(P)$ and the chemical potential of perfect gas $\mu_{\text{gas}}(P)$. The reference pressure is chosen to be the vapor pressure of water $P_{\text{water}}^{\text{vap}} = 5300 \text{ Pa}$ ⁴⁹ for which the chemical potential of water is set to zero. The chemical potential of perfect gas is written as follows

$$\mu_{\text{gas}}(P) = \frac{1}{\beta} \ln \left(\frac{P}{P_{\text{water}}^{\text{vap}}} \right) \quad (4)$$

where $\beta = \frac{1}{k_{\text{B}}T}$. The acceptance probability of insertion and deletion of a water molecule in a given system can be written as a function of pressure⁷⁵

$$\begin{aligned} \text{acc}(N_{\text{H}_2\text{O}} \rightarrow N_{\text{H}_2\text{O}} + 1) &= \min \left(1, \frac{V\beta\phi P}{N_{\text{H}_2\text{O}} + 1} e^{-\beta(U_{N_{\text{H}_2\text{O}}+1} - U_{N_{\text{H}_2\text{O}}})} \right) \\ \text{acc}(N_{\text{H}_2\text{O}} \rightarrow N_{\text{H}_2\text{O}} - 1) &= \min \left(1, \frac{N_{\text{H}_2\text{O}}}{V\beta\phi P} e^{-\beta(U_{N_{\text{H}_2\text{O}}-1} - U_{N_{\text{H}_2\text{O}}})} \right) \end{aligned} \quad (5)$$

where V is the volume of the system and ϕ the fugacity coefficient at pressure P . The chemical potential is related to the pressure of the reservoir by the $\mu_{\text{water}}(P)$ relationship, and it is more convenient to use pressure rather than chemical potential as input in a GCMC simulation, because chemical potential is defined from an arbitrary reference state. The fugacity coefficient ϕ appearing in eq 5 is the Boltzmann factor of the difference in chemical potential between the gas phase and the liquid phase denoted by $\Delta\tilde{\mu}(P)$ in Figure S11 at a given pressure P

$$\phi = e^{-\beta(\Delta\tilde{\mu}(P))} = e^{-\beta(\mu_{\text{gas}}(P) - \mu_{\text{water}}(P))} \quad (6)$$

which allows us to get rid of the reference state of the chemical potential because ϕ only depends on the relative difference of chemical potentials. Consequently, the chemical potential of liquid water is set to zero at vapor pressure. The fugacity f appearing in eq 5 is the product of the pressure and the fugacity coefficient

$$f = \phi P \quad (7)$$

If the input pressure P in eq 5 is below $P_{\text{water}}^{\text{vap}}$, water remains in its gaseous phase so that $\phi = 1$ and the pressure is indeed equal to fugacity. On the contrary, if the pressure is above $P_{\text{water}}^{\text{vap}}$, the fugacity coefficient drops ($\phi < 1$) and the fugacity is thus below the real pressure P . The fugacity f is the pressure that the hypothetical perfect fluid would have for its chemical potential to be the same as the chemical potential of the real fluid at pressure P .⁷⁵

Let us introduce the two following systems: the first one consists of a given zeolite in equilibrium with a reservoir of pure water, while the second system deals with the same zeolite, but the reservoir is replaced with an electrolyte solution. Then, a certain intrusion pressure P_{water} is required, resulting in an intrusion of a certain amount of water inside the zeolite of the first system, in equilibrium with the reservoir of water. Since we hypothesize that only water molecules are intruded/extruded in the zeolites in the presence of electrolyte solutions, we want to determine the intrusion pressure $P_{\text{water}}^{C_nA_m}$ that must be applied to the zeolite of the second system surrounding by the electrolyte solution, to obtain the same amount of intruded water molecules at equilibrium as for the first system. In order to find exactly the same number of water molecules in both zeolites, the probabilities in eq 5 must be the same for the two systems. In other words, it requires the fugacity of pure water f_{water} and water in the electrolyte solution $f_{\text{water}}^{C_nA_m}$ to be equal

$$f_{\text{water}} = f_{\text{water}}^{C_nA_m} \quad (8)$$

It has been shown that LiCl and NaCl electrolyte solutions have lower vapor pressure than pure water,⁷⁶ and assuming that chemical potential of water in electrolyte solutions has the same dependency in pressure as chemical potential of pure water, we plot respectively in Figure 7 the chemical potential of

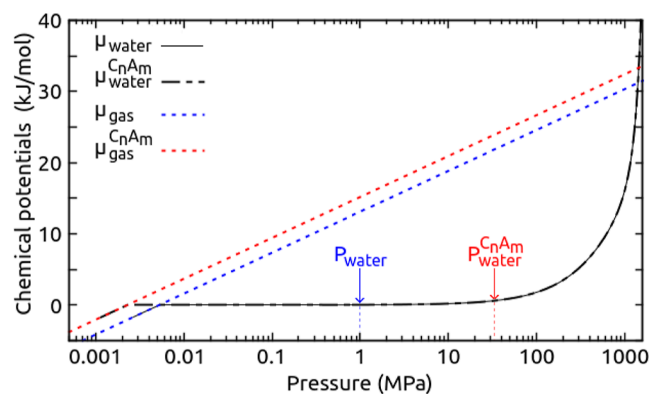


Figure 7. Chemical potential of pure water (full black curve) and water in electrolyte solution (dotted black curve) and respective curves of perfect gas in dotted blue and red lines. For instance, a hypothetical intrusion pressure P_{water} of 1 MPa (blue arrow) in a zeolite from a pure water reservoir corresponds to an intrusion pressure $P_{\text{water}}^{C_nA_m}$ of 33.5 MPa of water in the same zeolite, from the electrolyte solution reservoir, both characterized by the same acceptance probabilities of water intrusion (eq 5).

pure TIP4P water $\mu_{\text{water}}^{\text{pure}}(P)$ taken from Desbiens and co-workers for which $P_{\text{water}}^{\text{vap}}$ is equal to 5300 Pa and chemical potential of water in an electrolyte solution $\mu_{\text{water}}^{C_nA_m}(P)$ for which we choose a lower $P_{C_nA_m}^{\text{vap}}$ equals to 2300 as a proof-of-concept.

Hence, the $\mu_{\text{water}}^{C_n A_m}(P)$ relationship is simply the $\mu_{\text{water}}(P)$ relationship extended to $P_{C_n A_m}^{\text{vap}}$ so that we have $\mu_{\text{water}}^{C_n A_m}(P_{C_n A_m}^{\text{vap}})$ equals also to zero. Consequently, although the fugacities are equals (eq 8), the chemical potential of water in the electrolyte reservoir $\mu_{\text{water}}^{C_n A_m}(P)$ is thus different from the chemical potential of pure water reservoir $\mu_{\text{water}}(P)$. Let us rewrite eq 8 in term of pressure and fugacity coefficient

$$\phi_{\text{water}} P_{\text{water}} = \phi_{\text{water}}^{C_n A_m} P_{\text{water}}^{C_n A_m} \quad (9)$$

We introduce the difference of chemical potential between the real fluid and perfect gas in both sides, leading to the following expression

$$\begin{aligned} e^{-\beta(\mu_{\text{gas}}(P_{\text{water}}) - \mu_{\text{water}}(P_{\text{water}}))} P_{\text{water}} \\ = e^{-\beta(\mu_{\text{gas}}^{C_n A_m}(P_{\text{water}}^{C_n A_m}) - \mu_{\text{water}}^{C_n A_m}(P_{\text{water}}^{C_n A_m}))} P_{\text{water}}^{C_n A_m} \end{aligned} \quad (10)$$

The chemical potentials of the gas phase for both pure water and water in the presence of electrolyte are written as

$$\mu_{\text{gas}}(P) = \frac{1}{\beta} \ln \left(\frac{P}{P_{\text{water}}^{\text{vap}}} \right) \quad \mu_{\text{gas}}^{C_n A_m}(P) = \frac{1}{\beta} \ln \left(\frac{P}{P_{C_n A_m}^{\text{vap}}} \right) \quad (11)$$

Then, inserting eq 11 in eq 10 yields the following relationship

$$\mu_{\text{water}}(P_{\text{water}}) = \frac{1}{\beta} \ln \left(\frac{P_{C_n A_m}^{\text{vap}}}{P_{\text{water}}^{\text{vap}}} \right) + \mu_{\text{water}}^{C_n A_m}(P_{\text{water}}^{C_n A_m}) \quad (12)$$

Let us fit the chemical potentials $\mu_{\text{water}}(P_{\text{water}})$ and $\mu_{\text{water}}^{C_n A_m}(P_{\text{water}}^{C_n A_m})$ by a quadratic polynomial, to take into account of the increase of chemical potential and thus compression of water at high pressure

$$\begin{aligned} \mu_{\text{water}}(P_{\text{water}}) &= AP_{\text{water}}^2 + BP_{\text{water}} + C \\ \mu_{\text{water}}^{C_n A_m}(P_{\text{water}}^{C_n A_m}) &= A(P_{\text{water}}^{C_n A_m})^2 + BP_{\text{water}}^{C_n A_m} + D \end{aligned} \quad (13)$$

where A and B denote the same dependency of pressure for these chemical potentials, while C and D are different because we have chosen $\mu_{\text{water}}(P_{\text{water}}^{\text{vap}})$ and $\mu_{\text{water}}^{C_n A_m}(P_{C_n A_m}^{\text{vap}})$ to be equal to zero. The polynomials 13 are introduced in eq 12 in order to obtain a quadratic equation linking P_{water} and $P_{\text{water}}^{C_n A_m}$

$$\begin{aligned} A(P_{\text{water}}^{C_n A_m})^2 + BP_{\text{water}}^{C_n A_m} + \left(\frac{1}{\beta} \ln \left(\frac{P_{C_n A_m}^{\text{vap}}}{P_{\text{water}}^{\text{vap}}} \right) - AP_{\text{water}}^2 - BP_{\text{water}} \right. \\ \left. + D - C \right) = 0 \end{aligned} \quad (14)$$

The resolution of eq 14 provides an analytical relationship between P_{water} and $P_{\text{water}}^{C_n A_m}$

$$\begin{aligned} P_{\text{water}}^{C_n A_m} = \\ \frac{-B + \sqrt{(2AP_{\text{water}} + B)^2 - \frac{4A}{\beta} \ln \left(\frac{P_{C_n A_m}^{\text{vap}}}{P_{\text{water}}^{\text{vap}}} \right) + 4A(C - D)}}{2A} \end{aligned} \quad (15)$$

The above fits of polynomials 13 lead to values of $-1.44027 \times 10^{-6} \text{ kJ}\cdot\text{mol}^{-1}\cdot\text{MPa}^{-2}$; $1.74119 \times 10^{-2} \text{ kJ}\cdot\text{mol}^{-1}\cdot\text{MPa}^{-1}$;

$2.47448 \times 10^{-2} \text{ kJ}\cdot\text{mol}^{-1}$, and $2.47978 \times 10^{-2} \text{ kJ}\cdot\text{mol}^{-1}$ for A , B , C , and D coefficients. Consequently, the term $4A(C - D)$ is about $\sim 10^{-10} \text{ MPa}^2$, which is much lower than the other terms in the equation and thus can be ignored. This assumption is valid for any electrolyte solution in our model because it would have a vapor pressure lower than the vapor pressure of pure water. Also, the chemical potential profile is very flat at low pressure resulting in very close values of the constant coefficient of the quadratic fit for chemical potential of pure water C and for water in electrolyte solutions D . Therein, eq 15 becomes

$$P_{\text{water}}^{C_n A_m} \approx \frac{-B + \sqrt{(2AP_{\text{water}} + B)^2 - \frac{4A}{\beta} \ln(a_{\text{water}}^{C_n A_m})}}{2A} \quad (16)$$

where we introduce the activity of water in the electrolyte solution $a_{\text{water}}^{C_n A_m}$ being the ratio between $P_{C_n A_m}^{\text{vap}}$ and $P_{\text{water}}^{\text{vap}}$. Equation 16 is the analytical model used subsequently to predict the intrusion pressure of the electrolyte solutions in zeolites. In Figure 7, we select a hypothetical intrusion pressure P_{water} of 1 MPa from the pure water reservoir and deduce using eq 16 that the corresponding intrusion pressure of water from the electrolyte solution reservoir leading to the same acceptance probabilities of water intrusion (eq 5) is 33.5 MPa. This example shows qualitatively that a decrease of vapor pressure of a solution due to presence of electrolyte is consistent with a shift of intrusion pressure toward higher values. Our model requires as input the water activity in electrolyte solutions $a_{\text{water}}^{C_n A_m}$ over a wide range of concentration in order to rationalize intrusion pressure of electrolyte solutions in zeolites. There has been a large effort in order to obtain thermodynamic data (osmotic coefficient, activity coefficients...) of electrolyte solutions, either acquired experimentally to build theoretical models or through molecular simulations. The most widespread computational technique is the Gibbs ensemble MC method^{75,77–79} based on particle exchange between two reservoirs containing the two phases in equilibrium (e.g., liquid and vapor phase for water). Unfortunately, the Gibbs ensemble MC method in combination with the atomistic force field as used in our study make these simulations costly to predict precisely the vapor pressure of electrolyte solutions. Another approach is the grand canonical screening technique^{76,80} used to determine the point of liquid–vapor coexistence for systems in contact with vacuum. The vapor pressure of LiCl and NaCl has been obtained from screening various chemical potentials using GCMC simulations but using a coarse-grained description of electrolyte solutions. Consequently, this approach has the same limitation as that for the Gibbs ensemble MC method to be used in combination with atomistic force fields. Also, another straightforward approach used a modified Widom insertion method⁸¹ to compute the activity coefficient of electrolyte, but in implicit water solvation making it unsuitable for atomistic force field either. Theoretical models based on experimental thermodynamic data are alternative approaches to predict vapor pressure (and, by extension, activity of water) in electrolyte solutions. The Debye–Hückel theory provides analytical equations to calculate activity and osmotic coefficients, but its validity domains is about of $\sim 0.01 \text{ M}$ because of the neglect of short-range interactions, ion size and ion–ion correlations.⁸² There has been a huge effort devoted to extend the applicability range of the Debye–Hückel theory

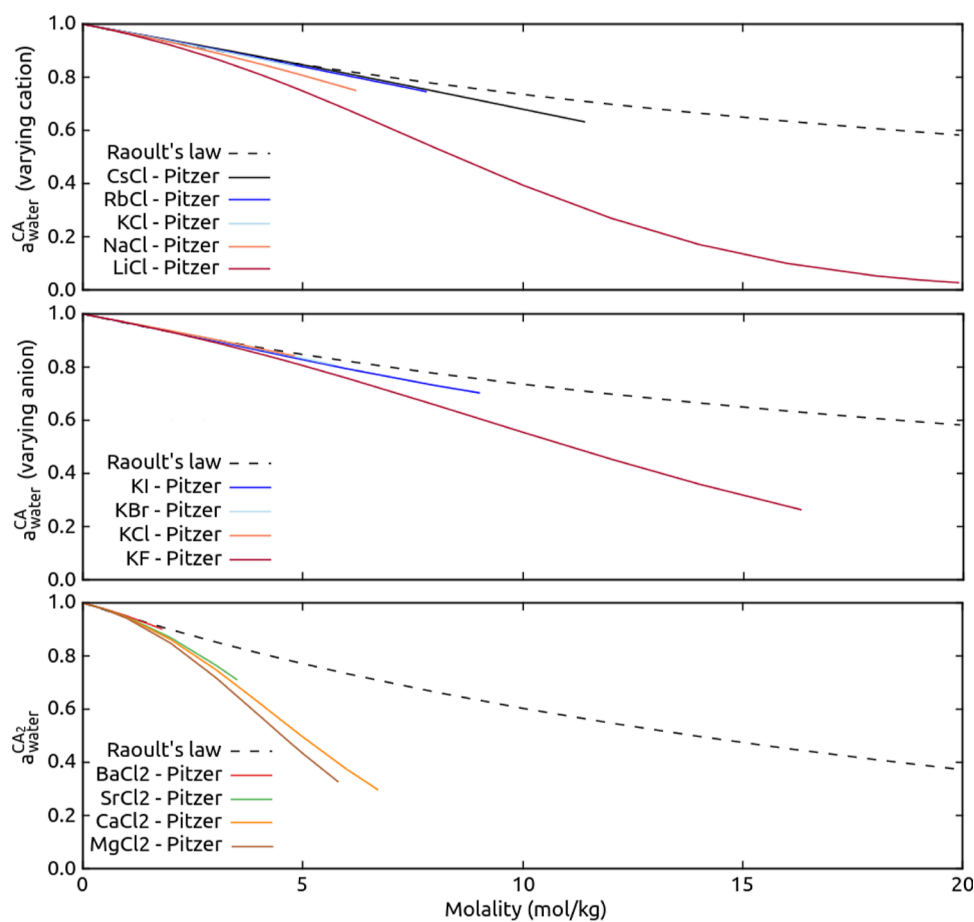


Figure 8. Activity of water in electrolyte solutions $a_{\text{water}}^{C_n A_m}$ up to saturation molality. Top: alkali–chloride electrolyte solutions; middle: potassium–halide electrolyte solutions; bottom: earth alkali–chloride electrolyte solutions. The dotted line indicates the activity coefficient obtained from Raoult's law.

by adding the above effects through fitting parameters. Along this line, the specific interaction theory^{83–85} uses experimental equilibrium constant at different ionic strength to determine activity coefficients for a wide range of concentration. A more sophisticated model has been proposed by Pitzer⁸⁶ by which activity and osmotic coefficients of single as well as mixed electrolytes at different temperatures can be modeled up to molalities of ~ 10 mol/kg, at the expense of a higher number of fitting parameters. We decided to use the Pitzer model in our work, not only because it is a sophisticated model that has been widely used in the literature but it also has been extended for various electrolyte combinations and concentrations.^{87–90} The version 0.5.2 of the Pytzer simulation package⁹¹ is the state-of-the-art summarizing the Pitzer parameters available in the literature for the series of electrolytes used in this work. We calculated with the Pytzer package the activity of water $a_{\text{water}}^{C_n A_m}$ (Figure 8) as well as the mean activity coefficient of electrolytes $\gamma_{C_n A_m}$ (Figures S12–S14) up to saturation molality for each electrolyte of our study (Table S8). We also provide raw data for all electrolytes in Tables S9–S20.

First, at low electrolyte molality, for all cases, the activity of water obeys Raoult's law. There is a clear correlation between a decrease of ion radius and deviation from the Raoult's law at high molality as shown by the drop of water activity for LiCl and KF electrolytes (top and middle panel of Figure 8). This is attributed to the higher solvation of water in the presence of

smaller ions⁵⁵ that contributes to lower activity of water and conversely increases activity coefficient of electrolytes $\gamma_{C_n A_m}$ (Figures S12–S14). Also, the effect of cation charge is clearly visible for divalent-cation electrolyte as water activity for all cases drops at low molality compared to monovalent electrolytes (bottom panel, Figure 8). Finally, the Pitzer model reproduces the experimental activity coefficient of electrolytes $\gamma_{C_n A_m}$ except up to 10 mol/kg for LiCl, so that we can use the values of $a_{\text{water}}^{C_n A_m}$ to predict intrusion pressure for electrolyte solutions in zeosils, knowing the intrusion pressure in pure water by using eq 16.

Prediction of Intrusion/Extrusion Pressure in Porous Materials. We introduced the above-mentioned analytical model in the context of zeosils, but it can be applied to various hydrophobic porous materials such as MOFs, provided that the same hypotheses are satisfied (i.e., no alteration of the porous material and only water molecules intruded inside it). We compare experimental data for intrusion pressure of various zeosils with prediction obtained from our analytical model and with the van't Hoff law of osmotic pressure expressed as follows

$$P_{\text{water}}^{C_n A_m} = P_{\text{water}} + imRT \quad (17)$$

where i is the number of ions per electrolyte unit, R is the ideal gas constant, T is the temperature and m the molality in mol/kg. For monovalent electrolytes, we have $i = 2$ and $iRT = 4.99$

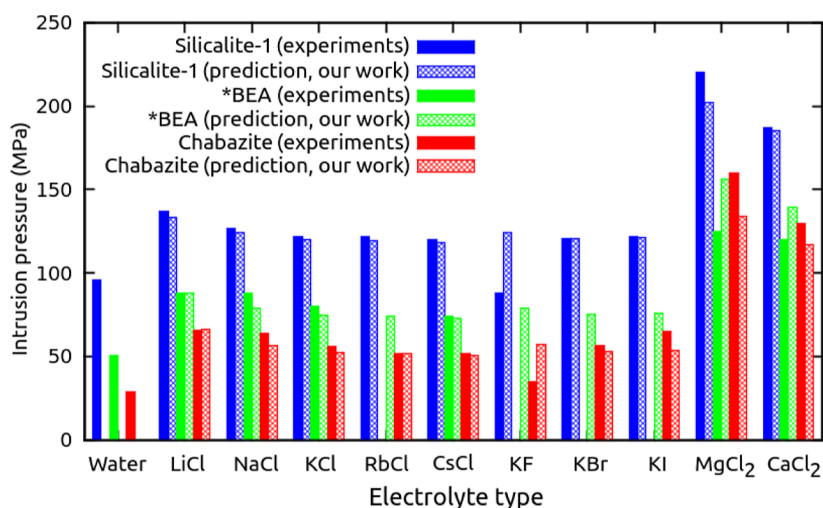


Figure 9. Intrusion pressure of water and electrolyte solutions (molality of 4.62 mol/kg) in silicalite-1 (blue), chabazite (red), and *BEA-type zeosil (green). Full histograms: experimental intrusion pressures; dashed histograms: predicted intrusion pressure with eq 16.

MPa·kg·mol⁻¹ while for divalent-cation electrolytes, we have $i = 3$ and $iRT = 7.48$ MPa·kg·mol⁻¹.

We screen intrusion pressure of different electrolyte solutions in three zeosils which are silicalite-1, chabazite, and *BEA-type zeosil. Figure 9 reports both experimental data and predictions from our model for a molality of 4.62 mol/kg, corresponding to a ratio of 12 water molecules per electrolyte unit C_nA_m . Our model reproduces experimental intrusion pressures except for KF where the experimental intrusion is much lower than predicted. This could be attributed to the formation of silanol defects upon the reaction of SiO₂ of HF acid appearing from hydrolysis of water due to F⁻ anions.

In Figure S15, we provide in addition the histogram of intrusion pressures predicted by the van 't Hoff law of osmotic pressure that both underestimates for most electrolytes the intrusion pressure and does not distinguish between electrolytes that produce the same ideal entropy of mixing, because at the studied concentration, electrolytes are non ideal as previously shown in Figure 8. The small variation of intrusion pressure existing within the series of electrolytes that can be rationalized in term of activity of water depends on the concentration and of the nature of the electrolyte, providing that input activity coefficients are properly parameterized. It is crucial from a practical point of view because at a given concentration, the electrolyte solution characterized by the lowest water activity such as LiCl results in the highest intrusion pressure and thus stored energy inside the material. This latter point is not taken into account by the van 't Hoff law for which electrolytes behave as ideal solutions.

CONCLUSIONS

We have investigated the electrolyte intrusion for various electrolyte solutions using molecular simulations and a revisited version of the law of osmotic pressure. We performed simulations on three representative pure-silica zeolites that are silicalite-1 (MFI type), chabazite (CHA type), and faujasite (FAU type) that were chosen to highlight the nature of the intruded fluid along their increasing pore diameter.

Before probing electrolyte intrusion, we reproduced by GCMC simulations the isotherm of water intrusion and extrusion for pure water in these zeosils and demonstrate that we reproduce intrusion pressures consistent with the literature.

Then, we used the equilibrated zeosils with the water reservoir at high pressure as the initial state to perform Monte Carlo simulations in the osmotic ensemble by using our version of the NCMC move. The alchemical work (i.e., the work performed by the system) for inserting a single electrolyte unit is associated with a very low probability of intrusion in silicalite-1 and chabazite while for faujasite, there could be intrusion of electrolyte because of the larger pore allowing a better solvation of the ions. The nonintrusion of electrolytes in the low-pore-diameter zeosils is consistent with experiments reporting only water as the first intruded species in chabazite and LTA-type zeosils.

Assuming that only water molecules penetrate in low-pore-diameter zeosils, we determined how the chemical potential of water evolves in the presence of electrolytes. By performing a series of MC simulations using our adapted NCMC move, we showed that the chemical potential of water in electrolyte solutions displays the same dependency in pressure as the chemical potential of pure water.

Finally, we revisit the law of osmotic pressure by proposing an analytical model for predicting the intrusion of water in zeosils. The shift of intrusion pressure toward greater values is directly induced by a drop of the activity of water and thus by a decrease of the vapor pressure of electrolyte solutions. The van 't Hoff law is not suited to calculate pressure beyond concentration of ~2 M because activity coefficient of water deviates from Raoult's law and depends clearly on the nature of the electrolyte of interest. Instead, we use the Pitzer model to calculate the activity of water for various electrolyte solutions up to saturation concentration. Our model was able to reproduce experimental intrusion pressures in various zeosils (silicalite-1, chabazite, and *BEA-type zeosil) for different electrolytes at relatively high concentration (molality of ~4.62 mol/kg), showing that our model accounts for both concentration and nature of the electrolyte solution. On the contrary, the van 't Hoff law of osmotic pressure assumes electrolyte solutions to be ideal and does not only reproduce the small variation of intrusion pressure existing in the presence of monovalent electrolytes but also clearly underestimates intrusion pressure for divalent-cation electrolytes. Hence, our model suggests that a high performance electrolyte for energy storage in nanoporous materials should have low

water activity to guarantee the highest intrusion pressure. We note, however, that the presence of silanol defects in zeosils increases their hydrophilicity and, therefore, decreases the intrusion pressure. In order to decipher the role of the silanol defects from the pore diameter on the intrusion pressure and the nature of the intruded fluid, we intend in the future to extend our methodology to more realistic zeosil models, including silanol defects.

■ ASSOCIATED CONTENT

SI Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/acs.chemmater.3c02230>.

Force field parameters, heat of adsorption of water in zeosils, raw data and the Supporting Information for alchemical work, chemical potentials, as well as activity coefficients (PDF)

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Notes

The authors declare no competing financial interest.

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